

# Enhanced in-plane magnetic anisotropy in thermally treated arrays of Co-Pt nanowires

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## Abstract

Ordered arrays of  $\text{Co}_x\text{Pt}_{100-x}$  cylindrical nanowires (NWs) with  $x=90, 80, 70$  were synthesized by template-assisted electrodeposition using nanoporous alumina membranes of 55 nm pore diameter. The obtained NWs alloys crystallize in *hcp* and/or *fcc* structures, depending on the composition and thermal treatment, resulting in different magnetic behaviors. The magnetic anisotropy was studied as a function of composition and crystalline structure in as-deposited and annealed samples. An enhanced coercivity was obtained for the  $\text{Co}_{70}\text{Pt}_{30}$  NWs array, in which in-plane anisotropy (e.g., perpendicular to the NWs axis) was found. These characteristics have not been reported for NWs of this kind. A simplified model of effective anisotropy including shape, magnetostatic interaction and magnetocrystalline contributions is presented, which appropriately describes the magnetic behavior of the  $\text{Co}_x\text{Pt}_{100-x}$  NWs arrays before and after annealing.

**Keywords:** Co-Pt alloys; Cylindrical Nanowires Arrays; Magnetic Anisotropy.

## 1. Introduction

Magnetic anisotropy is a key magnitude of ferromagnetic materials that determines their magnetic response in the presence of a magnetic field. Its origin is connected to the spin-orbit coupling at the atomic scale whose local symmetry is mainly determined by the composition of the material under consideration. Anisotropic magnetic materials are used in high-density magnetic recording applications [1–3], magneto-optic recording [4–6], micro- and nano-electromechanical devices (MEMS/NEMS) [7,8], magnetic actuators [9,10], sensors [11,12], spin valves [13,14], among others. In planar systems, sometimes perpendicular or out-of-plane anisotropy is desired, like in the case of high-density magnetic recording media. However, for a wide variety of applications it is convenient to engineer the magnetization easy direction defined by the magnetic anisotropy.

As a result of the investigation on hard magnetic materials, Co-based systems have improved with the addition of 4d or 5d noble metals, like Pd or Pt, respectively. The attribute of these alloys is the high magnetic moment—provided by Co— combined with the enhancement of the magnetic anisotropy, originated in the coupling of the Co-3d band with the noble metal 4d/5d band, which improves the orbital moments [15–17]. Particularly, when looking for highly anisotropic materials, Co-Pt alloys are better suited than Co-Pd or Co-X alloys, where X represents a 5d noble metal other than Pt [15,17].

Upon technological advances, Co-Pt-based devices have evolved from 3D bulk geometries [18,19] to low-dimensional nanostructures, like 2D thin films [20–22], 1D nanowires [23–25] and 0D nanoparticles [26–28]. The magnetic properties of these structures are strongly affected by the magnetic anisotropy, which can be considered as coming from different contributions. For example, for 0D nanostructures the magnetocrystalline anisotropy and the size of the particles are determinant features to control the magnetic properties [29,30]. In the case of higher dimensionality systems, shape anisotropy is also present, increasing possibility of tuning the magnetic anisotropy.

For 1D-like NWs arrays, the confinement to one dimension promotes the growth of crystalline phases and many synthesis methods are possible. For instance, thermal decomposition [31], solvothermal synthesis [25], and electrochemical routes like direct current (DC) [23,24,32–37] template-assisted electrodeposition. Electrochemistry has the advantage of employing simple and less-expensive equipment, while the suitable modification of its parameters offers a great versatility to control the geometry and composition of the NWs arrays.

Many authors have studied arrays of metallic NWs and obtained different results regarding the magnetization easy axis of the system. When the diameter of the wires is larger than 100 nm it is possible to design the magnetic anisotropy to be in-plane, out of plane or negligible (isotropic) [32,34,38]. The same versatility is possible when working with Co-Pt thin films [20,39,40]. However, in the case of Co-Pt NWs arrays with diameter smaller than 100 nm, only out-of-plane magnetic anisotropy (that is, parallel to the NWs axis) has been reported [23,36,41–43]. This geometrical aspect limits the applicability of nanowires with diameters  $\leq 100$  nm, which usually display larger coercivities than thicker ones and thin films, because of geometrical confinement [24].

In this work, cylindrical  $\text{Co}_x\text{Pt}_{100-x}$  NWs arrays with  $x=90, 80, 70$  and diameter of 55 nm were synthesized by DC electrodeposition using nanoporous alumina membranes as templates. The magnetic anisotropy was studied as a function of composition and crystalline structure in as-deposited samples and after thermal treatments. In-plane anisotropy (e.g., perpendicular to the NWs axis) was found for the  $\text{Co}_{70}\text{Pt}_{30}$  array, in which an enhanced coercivity was obtained, when comparing with Co-Pt arrays of thicker wires (diameter  $\geq 100$  nm) and thin films of compositions ranging from  $\text{Co}_{90}\text{Pt}_{10}$  to  $\text{Co}_{40}\text{Pt}_{60}$  [22,32,34,38,39,44–46].

## 2. Samples preparation and processing

The preparation of the Anodic Aluminum Oxide (AAO) templates was carried out by a two-step anodization process, as described previously [47,48]. These structures are characterized by an ordered hexagonal arrangement of cylindrical pores, with diameter  $d_{\text{pore}} = (55 \pm 5)$  nm, interpore distance (between pore centers)  $d_{\text{cc,pore}} = (110 \pm 10)$  nm and length  $L_{\text{pore}} = (40 \pm 2)$   $\mu\text{m}$ . A 200 nm thick gold layer is sputtered on one side of the template to make the electrical contact for electrodeposition. Figure 1 (a) (left) shows a top view of an AAO template.

Electrodeposition of Co-Pt NWs was performed with a 0.015 M  $\text{K}_2\text{PtCl}_6$  + 0.3 M  $\text{CoSO}_4$  + 0.2 M  $\text{H}_3\text{BO}_3$  solution, pH = 3.3, in a three-electrode cell. All the reagents were of analytical grade from Sigma-Aldrich. Since Co and Pt have very different reduction potentials (-0.28 V and 1.18 V vs. SHE at 25 °C and 1 atm, respectively [49]), the electrodeposition potential  $V$  was used to control the Co/Pt atomic ratio. The dependence of the composition  $\text{Co}_x\text{Pt}_{100-x}$  with  $V$  is non-linear, and for  $x = 90, 80, 70$  it was necessary to apply  $V = -0.8, -0.6$  and  $-0.5$  V (measured against a Ag/AgCl reference electrode), respectively. The electrodeposition time was fixed to 15 min because longer times led to irregular growing, generating a Pt deposition on the template's surface instead of within the pores.

After structural and magnetic characterization of the as-deposited samples, the NWs arrays were thermally treated looking for the stabilization of metastable phases and/or phase transitions. The annealing processes were carried out in a GSL-1700X furnace under Ar atmosphere with a +10 °C/min ramp from room temperature to 500 °C, 3 hours waiting time, and a -10 °C/min ramp to reach back room temperature.

## 3. Structural and magnetic characterization

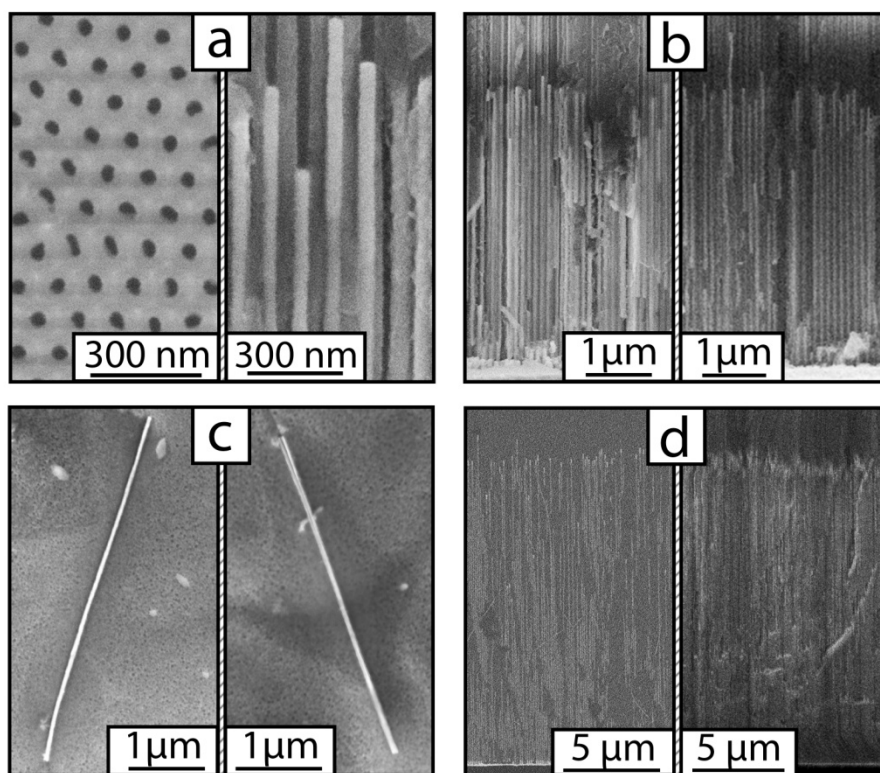
The synthesized NWs arrays were morphologically characterized with a Sigma Zeiss Field Emission Scanning Electron Microscope (FE-SEM). The NWs diameter  $d$  and center-to-center distance  $d_{\text{cc}}$  were pre-determined by the template (as verified from several SEM images),  $d = d_{\text{pore}} = (55 \pm 5)$  nm and  $d_{\text{cc}} = d_{\text{cc,pore}} = (110 \pm 10)$  nm. Despite having the same electrodeposition time, the NWs length  $L$  was different for each array because the electrodeposition potential  $V$  strongly affected the growing dynamics. For the lower values  $V = -0.6$  V and  $-0.5$  V, the length was approximately 4  $\mu\text{m}$ , while for  $V = -0.8$  V it was  $L \sim 16$   $\mu\text{m}$ . In all cases, the length-to-diameter ratio or aspect ratio  $Ar = L/d$  is large ( $\geq 70$ ).

The samples were labeled according to the Co content and whether they were annealed or not. For example, Co90-AD and Co90-TT represent the as-deposited (AD) and thermally treated (TT)  $\text{Co}_{90}\text{Pt}_{10}$  sample, respectively. Table 1 summarizes the morphological parameters of the as-deposited samples.

**Table 1.** Morphological and compositional parameters of the as-deposited nanowires arrays, with diameter  $d = (55 \pm 5)$  nm and interpore distance  $d_{\text{cc}} = (110 \pm 10)$  nm.

Sample	Length $L$ [ $\mu\text{m}$ ]	Aspect Ratio $Ar$	Co at. %	Pt at. %
Co90-AD	16 $\pm$ 1	290 $\pm$ 30	90 $\pm$ 3	10 $\pm$ 3
Co80-AD	4 $\pm$ 1	70 $\pm$ 20	80 $\pm$ 3	20 $\pm$ 3
Co70-AD	4 $\pm$ 1	70 $\pm$ 20	70 $\pm$ 3	30 $\pm$ 3

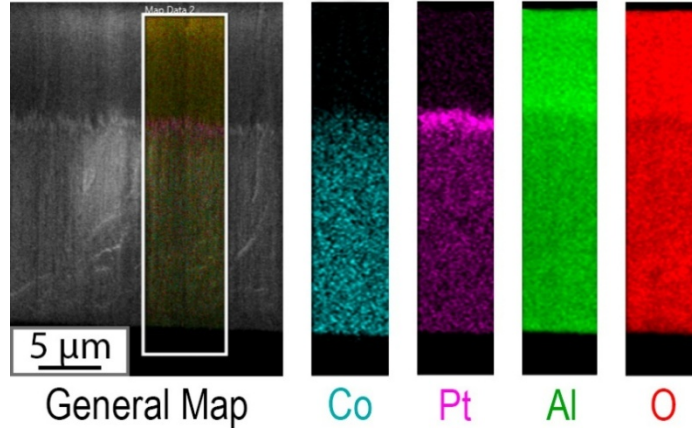
Figure 1 (a) (right) is a close-up SEM image of Co<sub>80</sub>-TT NWs within the AAO membrane, representative of all the arrays deposited in the template shown at the left side of this figure. Figure 1 (b) displays a SEM cross-section image of Co<sub>70</sub>-AD (left) and Co<sub>70</sub>-TT (right) NWs arrays. Single Co<sub>80</sub>-AD and Co<sub>80</sub>-TT nanowires on a silicon substrate, released from the template by chemical procedures are shown in Figure 1 (c) (left and right, respectively). Lastly, Figure 1 (d) (left) shows a backscattered electron (BSE) cross-section view of sample Co<sub>90</sub>-AD, in which the NWs, deposited Au layer and alumina template are visible, while a SEM image of the same array after thermal treatment is shown on the right. Comparison of the AD and TT samples indicates that the thermal treatment does not alter the morphology of the wires.



**Figure 1.** SEM images of: (a) top view of an AAO template (left) and Co<sub>80</sub>-AD NWs. (b) Cross-section view of sample Co<sub>70</sub>-AD (left) and Co<sub>70</sub>-TT (right). (c) Single Co<sub>80</sub>-AD (left) and Co<sub>80</sub>-TT (right) nanowire released from the template. (d) BSE cross-section view of sample Co<sub>90</sub>-AD (left) and SEM image of Co<sub>90</sub>-TT (right).

The elemental compositions  $\text{Co}_x\text{Pt}_{100-x}$  were measured for each sample with an Energy Dispersive Spectrometer (EDS) model APOLLO 10 SSD. Cobalt atomic contents  $x = 90, 80, 70$  were found for the voltages  $-0.8 \text{ V}, -0.6 \text{ V}$  and  $-0.5 \text{ V}$ , respectively (see Table 1). Figure 2 shows an elemental map from a section of the template corresponding to sample Co<sub>90</sub>-AD. The compositional distribution is clearly distinguished, and the alumina template is visible all across the length. In all investigated samples, Co and Pt are homogeneously distributed along the NWs length. The last few nanometers of the topmost segments present almost pure Pt tips, which may be a consequence of the potential cut off during the last stage of the electrodeposition. The tips protect the wires against oxidation while do not contribute to the magnetic behavior.

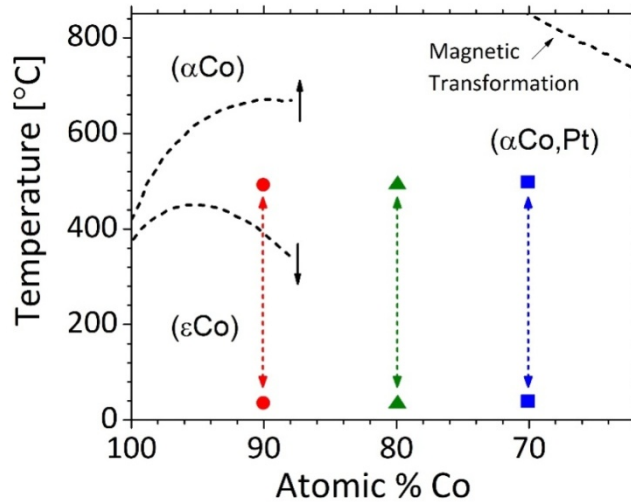
After annealing, not only the morphology remained unchanged (as seen in Figure 1) but also the composition, as determined by EDS studies.



**Figure 2.** Elemental EDS map of a section of a NWs array, corresponding to sample Co90-AD, where the nanowires and the alumina template are clearly distinguished.

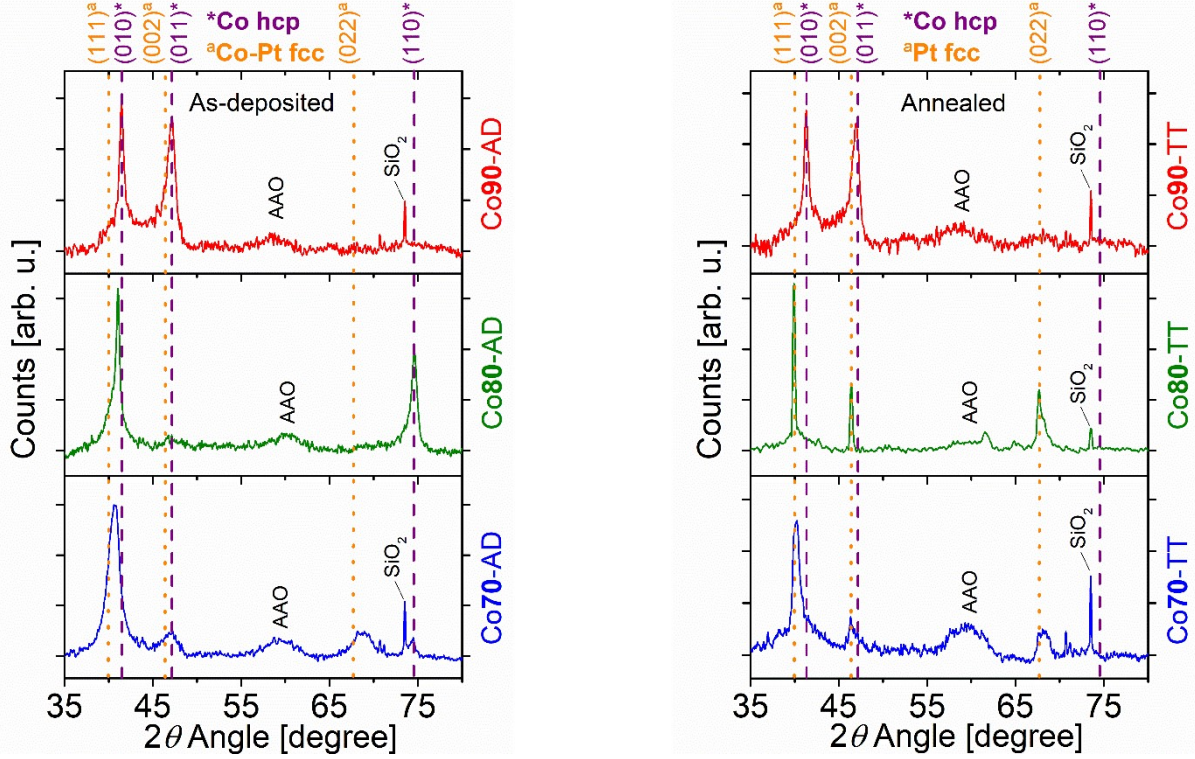
### 3.1 Crystalline Structure

The phase diagram for Co-Pt bimetallic alloy is well known for the bulk materials [50]. In the present study, the composition of the samples ( $\text{Co}_{90}\text{Pt}_{10}$ ,  $\text{Co}_{80}\text{Pt}_{20}$  and  $\text{Co}_{70}\text{Pt}_{30}$ ) and the annealing temperature (500 °C) limit the working zone to the region shown in Figure 3, where only two crystalline phases are possible: cubic *fcc* ( $\alpha\text{Co,Pt}$ ) or hexagonal *hcp* ( $\epsilon\text{Co}$ ). The *hcp* phase is more favorable when the Co content is high, above 90 at.% for temperatures below 600 °C. At at.% Co  $\leq 80$  and room temperature, the *hcp* phase becomes metastable whereas the *fcc* phase is energetically convenient [18,19,50]. The thermal evolution for each sample is indicated in the figure.



**Figure 3.** Co-Pt phase diagram in the working zone according to the obtained Co-Pt alloy compositions and annealing temperature (adapted from Reference [50]). The thermal evolution is indicated for each composition (synthesis at room temperature and annealing at 500 °C).

The crystalline structure of the samples was determined by wide-angle X-Ray Diffraction (XRD), performed with a Panalytical X'Pert Pro device, Cu long-fine focus PIXcel 1D detector, Cu  $K_\alpha$  radiation ( $\lambda = 1.5419 \text{ \AA}$ ) and instrumental width  $0.02^\circ$ . For these measurements, the NWs arrays embedded in the amorphous AAO templates were placed on a  $\text{SiO}_2$  sample holder. The XRD patterns of all samples are shown in Figure 4, where left and right panels correspond to as-deposited and thermally treated samples, respectively.



**Figure 4.** XRD patterns for as-deposited (left) and thermally treated (right) samples, with compositions  $\text{Co}_{90}\text{Pt}_{10}$ ,  $\text{Co}_{80}\text{Pt}_{20}$  and  $\text{Co}_{70}\text{Pt}_{30}$ . The vertical dotted lines (orange) correspond to the Pt *fcc* angular reflections, whereas the dashed lines (violet) belong to the Co *hcp* phase. The alumina and  $\text{SiO}_2$  sample holder present a broad peak at  $60^\circ$  and a sharp one at  $73^\circ$ , respectively.

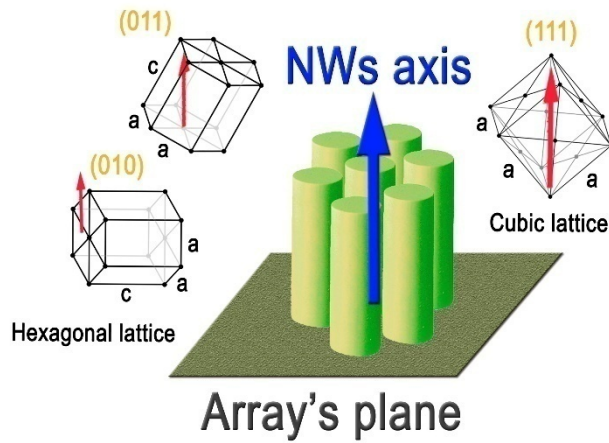
Before and after annealing, all the samples have polycrystalline structures. The Scherrer crystallite size  $d_s$  [51] was calculated using the peak with the highest intensity of each pattern, (010) for *hcp* and (111) for *fcc* structures. The obtained values are  $d_s = 10\text{-}20$  nm in every case, except in sample Co80-TT which shows a slight increase (30 nm). The lattice constants were experimentally determined from the Bragg's law and the geometry of each lattice [52], except for samples Co80-AD and Co70-AD due to the superposition of peaks in the *hcp* and *fcc* phases. The crystallographic texture was calculated from a comparison with powder diffraction patterns [53]. Table 2 presents these crystalline properties.

**Table 2.** Crystalline properties of all samples. The *hcp* / *fcc* notation indicates that the two crystallographic phases coexist. The associated textures and lattice parameters are also indicated.

Sample	Phase	$d_s$ [nm]	$a_{\text{exp}}$ [Å] [ $\pm 0.01\text{Å}$ ]	$c_{\text{exp}}$ [Å] [ $\pm 0.01\text{Å}$ ]	Texture
Co90-AD	<i>hcp</i>	10	2.48	4.13	(010),(011)
Co90-TT	<i>hcp</i>	10	2.48	4.14	(010),(011)
Co80-AD	<i>hcp</i> / <i>fcc</i>	20	2.50 / -	-	(010) / (111)
Co80-TT	<i>fcc</i>	30	3.85	$c = a$	None
Co70-AD	<i>hcp</i> / <i>fcc</i>	10	2.50 / -	-	-
Co70-TT	<i>fcc</i>	10	3.84	$c = a$	(111)

As expected from the phase diagram, sample Co90-AD crystallized in the Co *hcp* phase (PDF 96-901-1616) and remained unaltered after the thermal treatment (Co90-TT). It is possible that some Pt *fcc* grains are segregated in both cases, broadening the *hcp* peaks. The experimentally determined lattice constants are  $a_{\text{exp}} = (2.48 \pm 0.01)$  Å and  $c_{\text{exp}} = (4.13 \pm 0.01)$  Å for the basal and longitudinal directions, respectively, in both samples.

These values are close to the pure Co *hcp* lattice  $a_{\text{Co-hcp}} = 2.507 \text{ \AA}$  and  $c_{\text{Co-hcp}} = 4.069 \text{ \AA}$  [49], and the difference may arise from the bimetallic alloy or the peak broadening. The crystallographic texture is strong in both (010) and (011) *hcp* directions while the diffraction peak corresponding to the (002) *hcp* plane reflection (at  $44.486^\circ$ ) is missing. Therefore, there are no crystals oriented with the “c” axis of the hexagonal lattice parallel to the NWs axis, being most of the grains oriented along the (010) and (011) directions, as shown schematically in Figure 5.



**Figure 5.** Scheme of the ordered NWs within the template, indicating the direction of the NWs axis and the array's plane. Representative crystallographic images of *hcp* (left) and *fcc* (right) crystals are also displayed, positioned according to the observed textures in the samples. The arrows denote the NWs axis orientation.

In the case of sample Co80-AD, the peak at  $74.587^\circ$  corresponds to the (110) *hcp* reflection, and the one at  $41.044^\circ$  is very close to the (010) *hcp* direction, but also has a small contribution from the (111) Pt *fcc* reflection (PDF 96-901-3418). That is consistent with the metastability of the *hcp* phase for this composition at room temperature, and because this sample is not annealed, most of the grains are still in the hexagonal phase. Only the basal lattice constant  $a_{\text{exp}} = (2.50 \pm 0.01) \text{ \AA}$  for the *hcp* structure could be determined from the (110) *hcp* reflection. The crystallographic texture is associated to the (110) and (010) directions of the *hcp* phase, indicating that the “c” axis lays in the plane of the array for all grains, that is, perpendicular to the NWs axis.

After annealing, sample Co80-TT crystallized in the Pt *fcc* phase, accordingly with the phase diagram, with no crystallographic texture. There are no reflections corresponding to the *hcp* planes from Co, evidencing that Co and Pt are alloyed and the previous Co *hcp* and Pt *fcc* segregation disappeared. The lattice constant  $a_{\text{exp}} = (3.85 \pm 0.01) \text{ \AA}$  is close to the pure Pt value  $a_{\text{Pt}} = 3.912 \text{ \AA}$  [54].

Similarly to Co80-AD, sample Co70-AD also displays two contributions to the XRD pattern from the Co *hcp* and Pt *fcc* phases. As a result of the *hcp* and *fcc* peaks superposition, the reflections centered at  $40.720^\circ$  and  $47.164^\circ$  are quite broad. However, it is possible to verify that this sample is at least partially alloyed, because the *fcc* reflections are shifted with respect to the pure Pt lattice, as it can be observed in the (022) *fcc* reflection. The basal *hcp* lattice constant  $a_{\text{exp}} = (2.50 \pm 0.01) \text{ \AA}$  was determined from the small (110) *hcp* reflection. Due to the superposition of crystallographic phases there is no information about the other lattice parameters and an exact description of the crystallographic texture cannot be assessed.

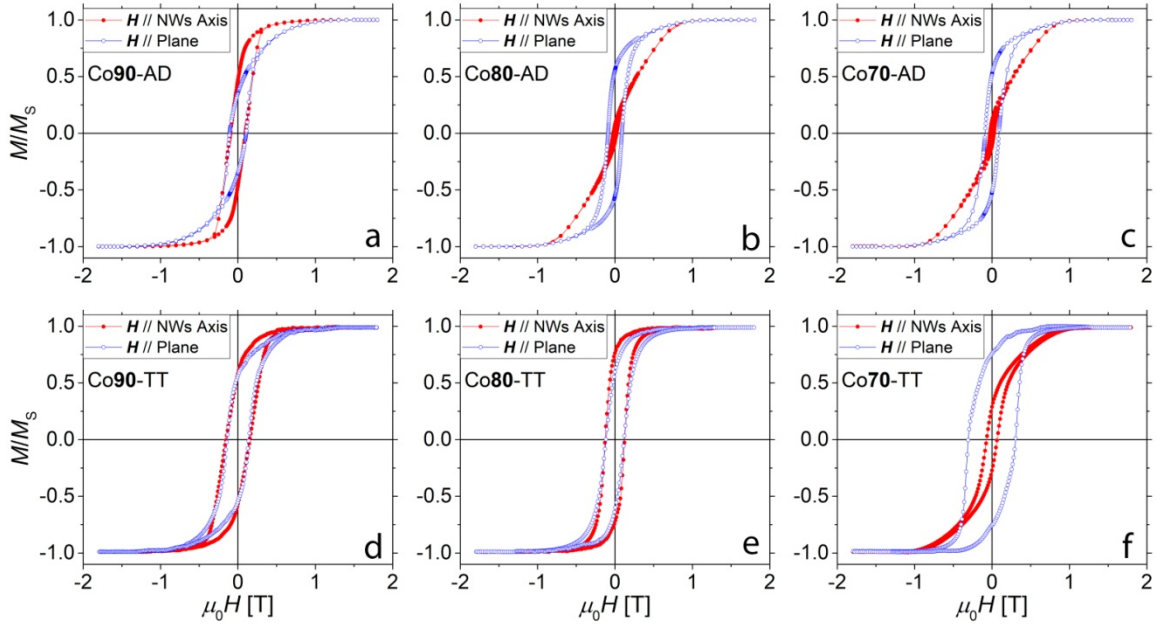
After the thermal treatment, sample Co70-TT adopts the Pt *fcc* structure, in agreement with the phase diagram, yet probably some Co *hcp* grains remain, according to the broad peaks at  $40.231^\circ$  and  $46.349^\circ$ . A crystallographic texture in the (111) direction is observed. The lack of intense peaks associated to the Co *hcp* phase confirms that Co and Pt are alloyed. The lattice constant is  $a_{\text{exp}} = (3.84 \pm 0.01) \text{ \AA}$ , similar to sample Co80-TT.

### 3.2 Magnetic Properties

The magnetic properties of the NWs arrays were determined in a Vibrating Sample Magnetometer (VSM, model ADE system EV7 KLATencor) with  $\mu_0 H^{\text{MAX}} = \pm 1.8 \text{ T}$  (being  $H^{\text{MAX}}$  the maximum applied field). The coercivity  $H_C$  and relative remanence  $m_R = M_R/M_S$ , ( $M_R$ =remnant magnetization;  $M_S$ =saturation magnetization) were obtained by analyzing the hysteresis loops before and after annealing. These measurements were carried out in a complete range of angles between the applied field  $H$  and the NWs axis, from  $0^\circ$  to  $180^\circ$ , being  $\theta=0^\circ$  the

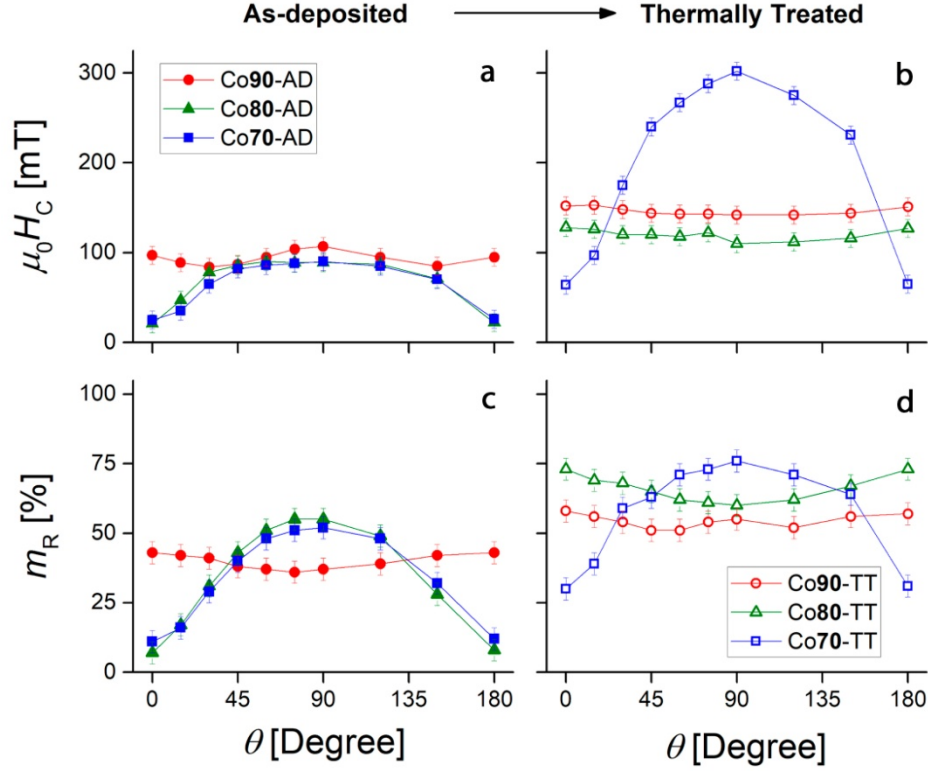
configuration of  $\mathbf{H}$  parallel to the NWs axis (i.e., out of plane) and  $\theta=90^\circ$  the perpendicular orientation (in the plane of the membrane).

Figure 6 shows  $\theta=0^\circ$  and  $\theta=90^\circ$  hysteresis loops of the as-deposited (top panel) and annealed (bottom panel) samples. Sample Co90-AD shows a net but small out-of-plane effective anisotropy, as it can be deduced from the increased value of remanence in the parallel field configuration,  $m_R(\theta=0^\circ)=0.46$  instead of  $m_R(\theta=90^\circ)=0.35$  (see Figure 6 (a)). On the other hand, samples Co80-AD and Co70-AD are remarkably similar and anisotropic (Figures 6 (b) and (c), respectively), with in-plane effective anisotropy. After annealing, samples Co90-TT and Co80-TT become almost isotropic (Figures 6 (d) and (e), respectively) while sample Co70-TT enhances its effective in-plane anisotropy (Figure 6 (f)).



**Figure 6.** Hysteresis loops (top panel) before and (bottom panel) after annealing of samples (a) Co90-AD, (b) Co80-AD, (c) Co70-AD, (d) Co90-TT, (e) Co80-TT and (f) Co70-TT with the applied field  $\mathbf{H}$  parallel to the NWs axis ( $\theta=0^\circ$ , solid circles) and parallel to the array's plane ( $\theta=90^\circ$ , open circles).

It is noteworthy that the magnetic behavior of the arrays changed after the annealing. Figure 7 displays both (top panel)  $\mu_0 H_C$  vs.  $\theta$  and (bottom panel)  $m_R$  vs.  $\theta$  curves for (a, c) as-deposited and (b, d) thermally treated samples. The relative remanence mimics the coercivity behavior in every sample, being both of them maximized at the same angles. The magnetization easy axis (MEA) can be taken as the direction in which the largest coercivity ( $H_C^{\text{MAX}}$ ) and relative remanence ( $m_R^{\text{MAX}}$ ) are attained. For samples Co80-AD, Co70-AD and Co70-TT both  $H_C^{\text{MAX}}$  and  $m_R^{\text{MAX}}$  occur at  $\theta=90^\circ$  (the array's plane). On the contrary, samples Co90-AD and Co90-TT show a rather constant behavior for  $H_C$  and  $m_R$ , being magnetically isotropic. Lastly, sample Co80-TT also presents a constant behavior for  $H_C$ , but  $m_R^{\text{MAX}}$  is attained at  $\theta=0^\circ$  (and  $\theta=180^\circ$ ), indicating that this is the direction of the MEA.



**Figure 7.**(Top panel) Coercivity and (bottom panel) relative remanence for the (a, c) as-deposited and (b, d) annealed NWs arrays as functions of the angle between the applied field and the NWs axis. As-deposited and thermally treated samples are represented by solid and open symbols, respectively. The compositions  $\text{Co}_{90}\text{Pt}_{10}$ ,  $\text{Co}_{80}\text{Pt}_{20}$  and  $\text{Co}_{70}\text{Pt}_{30}$  are associated to circles, triangles and squares, respectively.

For all the as-deposited samples,  $\mu_0 H_C^{\text{MAX}}$  was 100 mT when the field was applied parallel to the array's plane ( $\theta=90^\circ$ ). After the thermal treatment, this value increased only slightly for samples  $\text{Co}_{90}\text{-TT}$  and  $\text{Co}_{80}\text{-TT}$ , but it tripled ( $\mu_0 H_C^{\text{MAX}}=300$  mT) for  $\text{Co}_{70}\text{-TT}$ . After annealing,  $m_R^{\text{MAX}}$  also increased, around 20 % in every case. These magnetic parameters, as well as the corresponding MEA are summarized in [Table 3](#).

**Table 3.** Maximum values of coercivity and relative remanence, and the direction of the magnetization easy axis (MEA) for all samples.

Sample	$\mu_0 H_C^{\text{MAX}}$ [mT $\pm 10$ mT]	$m_R^{\text{MAX}}$ [% $\pm 3$ %]	MEA
$\text{Co}_{90}\text{-AD}$	100	43	Isotropic
$\text{Co}_{90}\text{-TT}$	150	58	Isotropic
$\text{Co}_{80}\text{-AD}$	100	56	$90^\circ$
$\text{Co}_{80}\text{-TT}$	130	73	$0^\circ$
$\text{Co}_{70}\text{-AD}$	100	52	$90^\circ$
$\text{Co}_{70}\text{-TT}$	300	76	$90^\circ$

#### 4. Discussion

To further understand the magnetic behavior of each sample, its correlation with the corresponding crystalline structure must be taken into account. The general behavior of a NWs array is determined by the individual energetic contribution of each nanowire plus an interaction term [55–63]. We consider the shape anisotropy  $K_{\text{shape}}$ , which depends on the geometry of a single nanowire, the interaction anisotropy  $K_{\text{inter}}$ ,



conditioned by the magnetostatic coupling of the NWs in the array, and the crystalline anisotropy  $K_{\text{crys}}$ , which is subordinated to the phase structure and crystallographic texture. The energy equilibrium equation can be reduced to an effective anisotropy  $K_{\text{eff}}$ , which represents the total energy density of the system:

$$K_{\text{eff}} = K_{\text{shape}} + K_{\text{inter}} + K_{\text{crys}} \quad (1)$$

Here, shape and interaction terms are of magnetostatic origin. The shape energy density  $K_{\text{shape}}$  is proportional to the squared saturation magnetization  $M_S^2$  and to the difference  $\Delta N$  of the demagnetizing factors parallel and perpendicular to the NWs axis [64]:

$$K_{\text{shape}} = \frac{1}{2} \Delta N \mu_0 M_S^2. \quad (2)$$

A positive value of  $K_{\text{shape}}$  means that the direction favored by this anisotropy is the NWs axis, whereas a negative result favors the array's plane. For the NWs arrays studied in this work  $\Delta N$  can be approximated by 0.5 (the maximum value for infinite cylindrical wires [64]) because of the high aspect ratio of the nanowires (see Table 1). For all samples, an upper bound for  $K_{\text{shape}}$  can be established using the saturation magnetization of pure Co ( $\mu_0 M_S = 1.79$  T [64]), giving  $K_{\text{shape}} = 637$  kJ/m<sup>3</sup> and favoring the NWs axis as the MEA.

The interaction anisotropy  $K_{\text{inter}}$  has been previously modeled according to different theories. Here, we follow the model proposed by Encinas-Oropesa et al. [61] for a hexagonal NWs array:

$$K_{\text{inter}} = -\frac{\sqrt{3}}{8} \pi \left( \frac{d}{dcc} \right)^2 \mu_0 M_S^2, \quad (3)$$

where the negative sign indicates that this anisotropy favors the alignment of the magnetization parallel to the array's plane. Using  $d = 55$  nm and  $dcc = 110$  nm, an upper bound for the interaction energy density for all samples can be estimated with the saturation magnetization of pure Co, giving  $K_{\text{inter}} = -434$  kJ/m<sup>3</sup> and promoting an easy plane of magnetization perpendicular to the NWs axis. Thus, these two energy terms compete to determine the MEA, resulting in a net magnetostatic energy constant of about  $K_0 = K_{\text{inter}} + K_{\text{shape}} \approx 203$  kJ/m<sup>3</sup> along the NWs axis.

The crystalline anisotropy  $K_{\text{crys}}$  depends on the crystal symmetry and texture. For single-crystal *hcp* pure Co it is  $K_{\text{crys}} \approx 450$  kJ/m<sup>3</sup> [65], which is of the same order of magnitude than the previously calculated  $K_{\text{shape}}$  and  $K_{\text{inter}}$ . In this case, the MEA is determined by the "c" axis orientation, which is also related to the texture. On the other hand, for textured *fcc* Co the crystalline anisotropy can also reach high values, up to 270 kJ/m<sup>3</sup> [66–68]. If the sample is polycrystalline with no crystallographic texture, then the crystalline energy averages to zero.

For samples Co90-AD and Co90-TT, the angular dependence of coercivity and relative remanence observed in Figure 7 indicates a nearly isotropic behavior. Considering the three energy terms taken into account for  $K_{\text{eff}}$  (Eq. 1), we infer that the magnetocrystalline anisotropy balances the magnetostatic terms. The NWs arrays show a hexagonal crystallographic symmetry with texture in the (010) and (011) directions along the NWs axis (see Figure 5), which favor, respectively, the MEA in the array's plane and the direction at a given angle with that plane. Given the polycrystalline character of the NWs, there is not any preferred azimuthal direction. We can estimate the effective magnetocrystalline anisotropy constant as  $K_{\text{crys}} \approx -200$  kJ/m<sup>3</sup> (i.e., in the array's plane), matching the magnitude of  $K_0$ . For this composition (Co<sub>90</sub>Pt<sub>10</sub>) the thermal treatment does not modify the isotropic behavior and both  $\mu_0 H_C$  and  $m_R$  are only moderately increased. This could be ascribed to a slight relaxation of the crystallographic structure while keeping the same texture.

As shown in Table 3, samples Co80-AD and Co80-TT are the only ones that display a MEA transition from in-plane (AD) to out-of-plane (TT). Before annealing, the main crystallographic phase of Co80-AD is Co *hcp* with the "c" axis laying in the array's plane ( $K_{\text{crys}} < 0$ ). In this sample, the MEA is in the array's plane as a result of the magnetocrystalline anisotropy overcoming the axial magnetostatic contribution ( $-K_{\text{crys}} > K_0$ ). After annealing, the crystalline structure completely transforms into cubic *fcc*, with no preferred crystallographic orientations. As a consequence, the magnetocrystalline anisotropy nearly vanishes and only the magnetostatic term  $K_0$  remains, leading to a MEA aligned with the NWs axis.

In both samples Co70-AD and Co70-TT the MEA lays in the array's plane, denoting an effective in-plane anisotropy. Therefore, the magnitude of  $K_{\text{crys}}$  overcomes  $K_0$  and has a negative value. It is noteworthy that even when both Co80-TT and Co70-TT show similar phase transitions to the *fcc* structure, Co80-TT has no preferential orientations, averaging  $K_{\text{crys}}$  to negligible values, while Co70-TT displays a crystallographic texture in the (111) direction which contributes to the enhanced in-plane magnetic anisotropy observed in this sample. Yamada et al. [22] found that for Co-Pt alloy thin films  $H_C$  shows a maximum at approximately 75 at.% Co content, both in-plane and in perpendicular directions. In the NWs arrays studied in this work, the maximum of effective magnetic

anisotropy this maximum is attained at a slightly lower Co content, the Co<sub>70</sub>Pt<sub>30</sub> composition, resulting in the large coercivity observed for sample Co70-TT. Before annealing (sample Co70-AD) there was a coexistence of *hcp* and *fcc* crystallographic phases preventing the magnetocrystalline anisotropy from reaching a higher value.

Summing up, shape anisotropy with an upper bound of  $K_{\text{shape}} \approx 640 \text{ kJ/m}^3$  always promotes a MEA in the NWs axis direction, while the interaction anisotropy  $K_{\text{inter}} \approx -440 \text{ kJ/m}^3$  (lower bound) favors a magnetization in the array's plane, and they compete to define the effective MEA. However, the magnetocrystalline anisotropy  $K_{\text{crys}}$  can balance or unbalance the equation depending on the crystalline phases and the crystallographic textures. Consequently, the magnetic effective anisotropy  $K_{\text{eff}}$  of the NWs array can be controlled by selecting the Co content –from 90 to 70 at.%– and the thermal treatment. Previous works on Co-Pt NWs arrays with diameter smaller than 100 nm never showed an in-plane magnetic anisotropy ( $K_{\text{eff}} < 0$ ). To the best of our knowledge, we are the first to achieve this feature for Co80-AD, Co70-AD and Co70-TT samples, which also present enhanced coercivity and remanence as compared to thicker NWs and thin films of different compositions, ranging from Co<sub>90</sub>Pt<sub>10</sub> to Co<sub>40</sub>Pt<sub>60</sub> [22,32,34,38,39,44–46].

## 5. Conclusion

Arrays of Co<sub>x</sub>Pt<sub>100-x</sub> ( $x = 90, 80, 70$ ) NWs of 55 nm diameter were synthesized by electrodeposition, using nanoporous alumina templates. Thermal treatments at 500 °C in Ar atmosphere were performed looking for the stabilization of metastable phases and phase transitions. The analysis of the crystalline phases for each sample showed that the *hcp* and/or *fcc* phases were obtained according to the composition and annealing, in agreement with the phase diagram for this alloy.

The magnetically isotropic behavior in samples Co90-AD and Co90-TT is ascribed to the balance between magnetostatic and crystalline terms in both samples. On the other hand, the in-plane magnetic anisotropy of sample Co80-AD is related to the *hcp* crystalline structure, textured in the array's plane, while after annealing (Co80-TT) the crystalline structure completely transforms into *fcc* phase with no crystallographic texture, resulting in a slightly anisotropic magnetic behavior, favoring the NWs axis direction. Samples Co70-AD and Co70-TT are textured in the array's plane, leading to an in-plane magnetic anisotropy. The remarkable hardening of Co70-TT may arise from the crystallographic transformation from *hcp* to *fcc* phase.

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## Data availability

The data that support the findings of this study are available on request from the corresponding author.

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